

HW#7 Solutions

1) In CM coordinates $\vec{L} = \sum_{\alpha} \vec{r}_{\alpha} \times \vec{p}_{\alpha} = \sum_{\alpha} m_{\alpha} \vec{r}_{\alpha} \times \dot{\vec{r}}_{\alpha} = \sum_{\alpha} m_{\alpha} \dot{\vec{r}}_{\alpha} \times (\vec{\omega} \times \vec{r}_{\alpha}) = \sum_{\alpha} m_{\alpha} \dot{\vec{r}}_{\alpha} \cdot (\vec{r}_{\alpha} \cdot \vec{\omega}) - \vec{r}_{\alpha} \cdot (\vec{\omega} \cdot \dot{\vec{r}}_{\alpha})$ ↙ using a standard double x-product identity

In component form: $L_i = \sum_{\alpha} m_{\alpha} (\omega_i \sum_k x_{\alpha k}^2 - x_{\alpha i} \sum_k \omega_k x_{\alpha k}) = \sum_{\alpha, k} (m_{\alpha} x_{\alpha k}^2 \omega_i - x_{\alpha i} x_{\alpha k} \omega_k)$

E.g.: $L_1 = \omega_1 (\sum_{\alpha} m_{\alpha} (x_{\alpha 1}^2 + x_{\alpha 2}^2 + x_{\alpha 3}^2) - m_{\alpha} x_{\alpha 1}^2) - \sum_{\alpha} m_{\alpha} x_{\alpha 1} (x_{\alpha 2} \omega_2 + x_{\alpha 3} \omega_3) = \omega_1 \sum_{\alpha} m_{\alpha} (x_{\alpha 2}^2 + x_{\alpha 3}^2) - \omega_2 \sum_{\alpha} m_{\alpha} x_{\alpha 1} x_{\alpha 2} - \omega_3 \sum_{\alpha} m_{\alpha} x_{\alpha 1} x_{\alpha 3}$
 $\qquad\qquad\qquad = \sum_k I_{1k} \omega_k$

Generally, $L_i = \sum_k I_{ik} \omega_k$

2) We have $m \left(\frac{d^2 \vec{r}}{dt^2} \right)_S = \vec{F}$ in the inertial frame and $\left(\frac{d^2 \vec{r}}{dt^2} \right)_S = \left(\frac{d^2 \vec{r}}{dt^2} \right)_s + \vec{\Omega} \times \vec{r}$ in non-inertial

$$\begin{aligned} \left(\frac{d^2 \vec{r}}{dt^2} \right)_S &= \left(\frac{d}{dt} \right)_S \left[\left(\frac{d \vec{r}}{dt} \right)_s + \vec{\Omega} \times \vec{r} \right] + \vec{\Omega} \times \left[\left(\frac{d \vec{r}}{dt} \right)_s + \vec{\Omega} \times \vec{r} \right] \\ &= \left(\frac{d^2 \vec{r}}{dt^2} \right)_s + \left(\frac{d \vec{\Omega}}{dt} \right)_s \times \vec{r} + 2 \vec{\Omega} \times \left(\frac{d \vec{r}}{dt} \right)_s + \vec{\Omega} \times (\vec{\Omega} \times \vec{r}) \end{aligned}$$

In N.I. frame: $m \ddot{\vec{r}} = \vec{F} + \underbrace{m \dot{\vec{r}} \times \vec{\Omega}}_{\text{azimuthal force term}} + 2m \vec{v} \times \vec{\Omega} + m (\vec{\Omega} \times \vec{r}) \times \vec{\Omega}$

3) If Coriolis + azimuthal forces are vanishing, then $m \ddot{\vec{r}} = \vec{F} + m (\vec{\Omega} \times (\dot{\vec{r}} \times \vec{\Omega})) = -mg_0 \hat{r} + m \Omega^2 r \sin \theta \hat{\rho}$

$\ddot{\vec{r}} = -g_0 \left[\hat{r} - \frac{m \Omega^2 r}{g_0} \sin \theta \hat{\rho} \right]$ At equator, $\hat{r} = \hat{\rho}$, and $\ddot{\vec{r}} = -g_0 \hat{r} \left[1 - \frac{m \Omega^2 r}{g_0} \right]$ ↑ free fall at N.P. ↑ unit vector away from axis (as in cylindrical coords)

generally $\ddot{\vec{r}} = -g_0 [\hat{r} + (\lambda - 1) \sin \theta \hat{\rho}] = -g_0 [\hat{r} + (\lambda - 1) \sin \theta (\sin \theta \hat{e} + \cos \theta \hat{\theta})]$
 $= -g_0 [(1 + (\lambda - 1) \sin^2 \theta) \hat{r} + (\lambda - 1) \sin \theta \cos \theta \hat{\theta}]$

Taking the magnitude: $g(\theta) = |\ddot{\vec{r}}| = g_0 [(1 + (\lambda - 1) \sin^2 \theta)^2 + (\lambda - 1)^2 \sin^2 \theta \cos^2 \theta]^{1/2}$

Simplifies to: $g(\theta) = \frac{g_0}{\sqrt{2}} [1 + \lambda^2 + (1 - \lambda^2) \cos 2\theta]^{1/2}$

4) We have $m \ddot{\vec{r}} = -mg \hat{z} + \vec{F}_c + 2m \dot{\vec{r}} \times \vec{\omega} + m (\vec{\omega} \times \vec{r}) \times \vec{\omega}$ which we must write in polar coordinates, taking $\dot{r} = 0$
↑ constraint force, to maintain bead on wire

$\ddot{\vec{r}} = \ddot{r} \hat{r} + r \ddot{\theta} \hat{\theta}$ $\ddot{\vec{r}} = (\ddot{r} - r \dot{\theta}^2) \hat{r} + (r \ddot{\theta} + 2 \dot{r} \dot{\theta}) \hat{\theta}$

Only keep track of $\hat{\theta}$ components, since \vec{F}_c always must nullify any other acceleration \rightarrow Coriolis force \perp to hoop \Rightarrow ignore

$m \ddot{\vec{r}} \rightarrow m r \ddot{\theta} \hat{\theta} = -mg \sin \theta \hat{\theta} + m \omega^2 R \sin \theta \cos \theta \hat{\theta}$

$\ddot{\theta} = -\frac{g}{R} \sin \theta \left(1 - \frac{\omega^2 R}{g} \cos \theta \right)$